

## **TILTED RECORDING MEDIUM WITH L<sub>10</sub> MAGNETIC LAYER**

### **Related Applications**

[0001] This application claims benefit from Provisional Application Serial No. \_\_\_\_\_, requested for conversion into a provisional application on July 28, 2003, from Application Serial No. 10/611,663, filed July 2, 2003, the entire disclosures of the above mentioned applications are hereby incorporated herein by reference.

### **Field of Invention**

[0002] This invention relates to magnetic recording media, such as thin film magnetic recording disks, and to a method of manufacturing the media. The invention has particular applicability to high areal density longitudinal magnetic recording media having very low medium noise.

### **Background**

[0003] Magnetic discs and disc drives provide quick access to vast amounts of stored information. Both flexible and rigid discs are available. Data on the discs is stored in circular tracks and divided into segments within the tracks. Disc drives typically employ one or more discs rotated on a central axis. A magnetic head is positioned over the disc surface to either access or add to the stored information. The heads for disc drives are mounted on a movable arm that carries the head in very close proximity to the disc over the various tracks and segments.

[0004] Figure 1 shows the schematic arrangement of a magnetic disk drive 10 using a rotary actuator. A disk or medium 11 is mounted on a spindle 12 and rotated at a predetermined speed. The rotary actuator comprises an arm 15 to which is coupled a suspension 14. A magnetic head 13 is mounted at the distal end of the suspension 14.

The magnetic head 13 is brought into contact with the recording/reproduction surface of the disk 11. A voice coil motor 19 as a kind of linear motor is provided to the other end of the arm 15. The arm 15 is swingably supported by ball bearings (not shown) provided at the upper and lower portions of a pivot portion 17.

**[0005]** A cross sectional view of a longitudinal recording disk medium is depicted in Figure 2. A longitudinal recording medium typically comprises a non-magnetic substrate 20 having sequentially deposited on each side thereof an underlayer 21, 21', such as chromium (Cr) or Cr-containing, a magnetic layer 22, 22', typically comprising a cobalt (Co) -base alloy, and a protective overcoat 23, 23', typically containing carbon. General practices also comprise bonding a lubricant topcoat (not shown) to the protective overcoat. Underlayer 21, 21', magnetic layer 22, 22', and protective overcoat 23, 23', are typically deposited by sputtering techniques. The Co-base alloy magnetic layer deposited by techniques normally comprises polycrystallites epitaxially grown on the polycrystal Cr or Cr-containing underlayer.

**[0006]** A longitudinal recording disk medium is prepared by depositing multiple layers of films to make a composite film. In sequential order, the multiple layers typically comprise a non-magnetic substrate, one or more underlayers, one or more magnetic layers, and a protective carbon layer. Generally, a polycrystalline epitaxially grown cobalt-chromium (CoCr) alloy magnetic layer is deposited on a chromium or chromium-alloy underlayer.

**[0007]** Methods for manufacturing a longitudinal magnetic recording medium with a glass, glass-ceramic, Al or Al-NiP substrate may also comprise applying a seed layer between the substrate and underlayer. A seed layer seeds the nucleation of a particular

crystallographic texture of the underlayer. A seed layer is the first deposited layer on the non-magnetic substrate. The role of this layer is to texture (alignment) the crystallographic orientation of the subsequent Cr-containing underlayer.

[0008] Conventionally, the seed layer, underlayer, and magnetic layer are sequentially sputter deposited on the substrate in an inert gas atmosphere, such as an atmosphere of argon. A carbon overcoat is typically deposited in argon with nitrogen, hydrogen or ethylene. Lubricant topcoats are typically about 20Å thick.

[0009] A substrate material conventionally employed in producing magnetic recording rigid disks comprises an aluminum-magnesium (Al-Mg) alloy. Such Al-Mg alloys are typically electrolessly plated with a layer of NiP at a thickness of about 10 microns to increase the hardness of the substrates, thereby providing a suitable surface for polishing to provide the requisite surface roughness or texture.

[0010] Other substrate materials have been employed, such as glass, e.g., an amorphous glass, glass-ceramic material that comprises a mixture of amorphous and crystalline materials, and ceramic materials. Glass-ceramic materials do not normally exhibit a crystalline surface. Glasses and glass-ceramics generally exhibit high resistance to shocks.

[0011] Longitudinal magnetic recording media having Cr<200> and Co<11.0> crystallographic preferred growth orientations (hereafter orientations) are usually referred as bi-crystal media, and are commonly used in the industry. Here, Cr<200> refers to bcc (body centered cubic) structured Cr-alloy underlayer or B2-structured underlayer with <200> preferred orientation. Typical bi-crystal media comprise Cr-containing alloy underlayers and Co-alloy magnetic layers. Cr-containing alloy has body centered cubic

crystalline structure. Uni-crystal media, which have  $\text{Co}\langle 10.0 \rangle$  preferred orientations and randomly oriented media have also been used. Perpendicular magnetic recording media having  $\text{Co}\langle 0002 \rangle$  preferred orientation are also being used. All of these media types typically have at least one small grain, hexagonal-closed-packed (hcp) Co-alloy magnetic layer with low exchange coupling.

**[0012]** The increasing demands for higher areal recording density impose increasingly greater demands on thin film magnetic recording media in terms of coercivity ( $H_c$ ); remanent coercivity ( $H_r$ ); magnetic remanance ( $M_r$ ), which is the magnetic moment per unit volume of ferromagnetic material; coercivity squareness ( $S^*$ ); signal-to-medium noise ratio (SMNR); and thermal stability of the media. These parameters are important to the recording performance and depend primarily on the microstructure of the materials of the media. For example, decreasing the grain size or reducing exchange coupling between grains, can increase SMNR, but it has been observed that the thermal stability of the media often decreases.

**[0013]** The requirements for high areal density, e.g. higher than  $100 \text{ Gb/in}^2$ , impose increasingly greater requirements on magnetic recording media in terms of coercivity, remanent squareness, medium noise, track recording performance and thermal stability. It is extremely difficult to produce a magnetic recording medium satisfying such demanding requirements, particularly a high-density magnetic rigid disk medium for longitudinal and perpendicular recording.

**[0014]** As the storage density of magnetic recording disks has increased, the product of  $M_r$  and the magnetic layer thickness ( $t$ ) has decreased and  $H_r$  of the magnetic layer has increased. This has led to a decrease in the ratio  $M_r t / H_r$ . To achieve a reduction in  $M_r t$ ,

the thickness  $t$  of the magnetic layer has been reduced, but only to a limit because the magnetization in the layer becomes susceptible to thermal decay.

**[0015]** Medium noise in thin films is a dominant factor restricting increased recording density of high-density magnetic hard disk drives, and is attributed primarily to inhomogeneous grain size and intergranular exchange coupling. Accordingly, in order to increase linear density, medium noise must be minimized by suitable microstructure control.

**[0016]** Longitudinal magnetic recording media containing cobalt (Co) or Co-based alloy magnetic films with a chromium (Cr) or Cr alloy underlayer deposited on a non-magnetic substrate have become the industry standard. For thin film longitudinal magnetic recording media, the desired crystallized structure of the Co and Co alloys is hexagonal close packed (hcp) with uniaxial crystalline anisotropy and a magnetization easy direction along the c-axis that lies in the plane of the film. The better the in-plane c-axis crystallographic texture, the more suitable is the Co alloy thin film for use in longitudinal recording to achieve high remanance and coercive force. For very small grain sizes, coercivity increases with increased grain size. The large grains, however, result in greater noise. Accordingly, there is a need to achieve high coercivities without the increase in noise associated with large grains. In order to achieve low noise magnetic recording media, the Co alloy thin film should have uniform small grains with grain boundaries capable of magnetically isolating neighboring grains thereby decreasing intergranular exchange coupling. This type of microstructural and crystallographic control is typically attempted by manipulating the deposition process, and properly using of underlayers and seedlayers.

[0017] It is recognized that the magnetic properties, such as Hcr, Mr, S and SMNR, which are critical to the performance of a magnetic alloy film, depend primarily upon the microstructure of the magnetic layer, which, in turn, is influenced by the underlying layers, such as the underlayer. It is also recognized that underlayers having a fine grain structure are highly desirable, particularly for growing fine grains of hcp Co alloys deposited thereon.

[0018] For high signal to noise ratio (SNR) magnetic recording media, it is desirable to have a high signal in a very thin film. Higher signal can be achieved by increasing the saturation magnetization (Ms) of the material at the top of the magnetic layer, and correspondingly increasing the fringing magnetic field that provides signal. Prior art magnetic recording systems generally employ media including a magnetic layer alloy including Co and Cr, and other elements often including Pt, and B. These magnetic layer systems generally require 10-25% Cr, and often use 5-15% B in order to isolate the magnetic grains in the magnetic layer and reduce noise.

[0019] There exists a continuing need for high areal density magnetic recording media exhibiting high Hcr and high SMNR while overcoming the deficiencies of the prior art solutions. In general, tilted magnetic recording is expected to overcome the deficiencies of the prior art because the head writes more efficiently upon media with magnetic easy axis tilted at an angle out-of-plane of the media surface. The tilted media recording system should thus be able to use higher Hc media. Tilted c-axis L<sub>10</sub> structures can provide a high Hc tilted media.

## **Summary of the Invention**

**[0020]** The invention relates to a recording medium and method of manufacturing the medium. The medium comprises a magnetic layer comprising a magnetic material comprising an ordered, face-centered tetragonal (fct)  $L_{10}$  structure having a c-axis of the fct  $L_{10}$  structure magnetic layer at an angle, canted about  $35^\circ$  out-of-plane of the magnetic layer. The fct  $L_{10}$  ordered structure is not based on a hcp structure but is based on a tetragonal structure. Current recording media designs utilize magnetization with easy axis either in the disk plane (longitudinal recording) or perpendicular to the disk plane (perpendicular recording) for storing data. This invention produces a recording medium with the easy magnetization axis lying about  $35^\circ$  tilted out-of-plane. Media SNR could be greatly improved from conventional longitudinal and perpendicular recording, because of an increase in the grain anisotropy that could be effectively written due to the angled recording configuration. A medium structure design to achieve this tilted magnetization configuration is disclosed. The medium of this invention could be used with a head designed for longitudinal or perpendicular recording.

**[0021]** One embodiment is a magnetic recording medium comprising (a) a magnetic layer comprising grains and (b) an underlayer comprising an underlayer material having a hcp or face-centered-cubic (fcc) lattice structure with a  $\langle 0002 \rangle$  or  $\langle 111 \rangle$  growth orientation, wherein at least two-thirds or more of the grains of the magnetic layer have a face-centered tetragonal (fct)  $L_{10}$  lattice structure having a c-axis that is at an angle, canted out-of-plane of the magnetic layer. Preferably, the underlayer has substantially no material having a  $L_{10}$  lattice structure and the unordered precursor material that is transformed into the  $L_{10}$  magnetic layer comprises an alloy having a fcc  $\langle 111 \rangle$  growth

orientation and is selected from the group consisting of substantially equiatomic CoPt, FePt, CoPd and FePd and mixtures of those alloys. Preferably, the fcc magnetic layer precursor material is annealed to form a magnetic layer having elemental composition similar to the precursor and having the fct  $L_{10}$  lattice structure. More preferably, the c-axis is canted about  $35^\circ$  out-of-plane of the magnetic layer, nearly parallel to a fcc  $\langle 001 \rangle$  axis of an underlayer or prior precursor grain. In one variation, the lattice structure of the underlayer material substantially matches the fct  $L_{10}$  lattice structure of the grains of the magnetic layer. Preferably, a mismatch between the hcp  $\{0002\}$  or  $\{111\}$  lattice plane of the underlayer material and the  $\{111\}$  plane of the fct  $L_{10}$  lattice structure of the grains of the magnetic layer is less than 10%. In one variation, the underlayer is directly in contact with the magnetic layer. Preferably, the underlayer material is one of a hcp material and a fcc material, commonly including a Ru alloy, a Ag alloy, a Pt alloy, or a Pd alloy. More preferably, the underlayer is on an amorphous TiCr alloy.

**[0022]** Another embodiment is a method of manufacturing a magnetic recording medium comprising (a) depositing an underlayer comprising an underlayer material having a hcp or fcc lattice structure with a  $\langle 0002 \rangle$  or  $\langle 111 \rangle$  growth orientation on a substrate and (b) subsequently depositing a magnetic layer comprising grains on the substrate, wherein at least two-thirds or more of the grains have a fct  $L_{10}$  lattice structure having a c-axis that is at an angle, canted out-of-plane of the magnetic layer.

**[0023]** Still another embodiment is a magnetic recording medium, comprising a substrate and means for producing an easy magnetization axis tilted away from a plane of the substrate. The means for producing an easy magnetization axis tilted away from the plane of the substrate surface are disclosed in several embodiments described below.



[0024] As will be realized, this invention is capable of other and different embodiments, and its details are capable of modifications in various obvious respects, all without departing from this invention. Accordingly, the drawings and description are to be regarded as illustrative in nature and not as restrictive.

### **Brief Description of the Drawings**

[0025] Figure 1 is a view of a magnetic disk drive.

[0026] Figure 2 is a schematic representation of the film structure in accordance with a magnetic recording medium of the prior art.

[0027] Figure 3 shows crystal lattice planes of a hexagonal closed packed structure.

[0028] Figure 4 shows crystal lattice planes of a face-centered cubic structure.

[0029] Figure 5 shows embodiments of the film structure according to the current invention.

### **Detailed Description**

[0030] In this application, the word “containing” means that the layer comprises the elements or compounds before the word “containing,” but the layer could still include other elements and compounds. Also, in this application, E-containing alloy and E alloy mean the same, where E is any element.

[0031] The recording medium of the invention may be a rigid magnetic disc rotatable about an axis that is incorporated into a disc drive shown in Figure 1. Disc drives such as this are standard equipment in the industry. See, Mee, C. D. and Daniel, E. D., MAGNETIC RECORDING, Vols. I-III (McGraw-Hill pub. 1987); F. Jorgenson, The Complete Handbook of Magnetic Recording, Chapter 16 (3rd. ed. 1988), and U.S. Pat. No. 5,062,021, the relevant disclosures of which are incorporated herein by reference.

The magnetic recording medium of the present invention may also be used with flexible magnetic discs or tapes using known flexible substrates.

[0032] Signal to noise ratio (SNR) of magnetic recording can be improved by increasing the maximum media coercivity for which a head can write magnetic transitions onto the media. It has been proposed in a related application Attorney Docket No. 146712004100 that media can be written at much higher coercivity when having magnetic grains with magnetic easy axis at an angle tilted near 45° away from the applied magnetic field. It is thus desirable to form high anisotropy magnetic recording media with easy axis tilted off of the film growth normal by a uniform amount, preferably near 45°.

[0033] This invention provides a magnetic recording medium suitable for high areal recording density exhibiting high thermal stability and high SMNR. This invention achieves such technological advantages by using high anisotropy compositionally ordered, face-centered tetragonal (fct)  $L_{10}$  structures such as CoPt, FePt, CoPd, FePd and their alloys. These materials have their easy axis parallel to the long c-axis of the tetragonal structure,  $\langle 001 \rangle$  and grow with the c-axis in-plane for longitudinal recording or out-of-plane for perpendicular recording. In this invention, these materials and similar materials are utilized such that the c-axis of the fct  $L_{10}$  structure of the magnetic layer is oriented at an angle, canted about 35° out-of-plane. Some embodiments of the invention enable tilted magnetic recording of a high coercivity magnetic medium by a perpendicular recording head.

[0034] Different crystallographic lattice planes of the hcp lattice of Co are shown in Figure 3. Figure 4 shows different lattice planes to the fcc lattice. By using an

appropriate underlayer, an fcc layer in a  $\langle 111 \rangle$  growth orientation or an hcp layer in a  $\langle 0002 \rangle$  growth orientation is grown by epitaxy or by graphoepitaxy, or by closest packed planes of the fcc or hcp layer having lowest interface energy with the substrate. The face centered cubic structure shown in Figure 4 encompasses pure elements having a fcc structure, as well as solid solutions of those pure elements and alloys.  $L_{10}$  is not a cubic structure.  $L_{10}$  is a derivative structure of fcc, which is not fcc lattice structure and has a c-axis that is at an angle, canted out-of-plane of the magnetic layer. Orienting the fcc precursor with the fcc underlayer so that the resulting special c-axis of the transformed  $L_{10}$  aligns with the fcc cube face of the underlayer is one important aspect of this invention.

**[0035]** As shown in Figures 3 and 4, the hcp  $\{0002\}$  and fcc  $\{111\}$  lattice planes comprise identical 2-dimensional structures, close-packed planes. Materials such as equiatomic CoPt, FePt, CoPd, FePd and mixtures thereof, can have a fcc crystal structure after sputter deposition at temperatures below 400°C. These materials, when grown on an appropriately lattice matched underlayer  $\{0002\}$  or  $\{111\}$  close-packed-plane, can thus be made to have a  $\langle 111 \rangle$  growth orientation.

**[0036]** Materials such as CoPt, FePt, CoPd, FePd transform from fcc to an ordered tetragonal  $L_{10}$  structure at high temperature, often above about 600°C. During the fcc to fct transition, the fcc  $\{111\}$  close-packed-plane is distorted into a lower symmetry closest packed fct  $\{111\}$  plane, but the fct  $\langle 111 \rangle$  direction is maintained parallel to the pre-transformation fcc  $\langle 111 \rangle$  growth direction. Thus, the resulting transformed fct  $L_{10}$  structure also has its  $\langle 001 \rangle$  c-axis nearly parallel to a pre-transformation  $\langle 001 \rangle$  axis.

[0037] A protective overcoat layer generally is deposited subsequent to the magnetic layer. The thickness of the protective layer could be about 10 Å to about 100 Å, preferably less than about 40 Å. The protective layer could be a carbon-containing layer, and may in some embodiments be made of hydrogenated carbon, nitrogenated carbon, hybrid carbon, or a combination of them.

[0038] The carbon overcoat could be further coated with a lubricant layer generally 1 nm to 2 nm thick. The lubricant is preferably a fluorocarbon or a perfluoroether. Examples include  $\text{CCl}_2\text{FCClF}_2$ ,  $\text{CF}_3(\text{CF}_2)_4\text{CF}_3$ ,  $\text{CF}_3(\text{CF}_2)_5\text{CF}_3$ ,  $\text{CF}_3(\text{CF}_2)_{10}\text{CF}_3$ , and  $\text{CF}_3(\text{CF}_2)_{16}\text{CF}_3$ .

[0039] The substrates that may be used in the invention include Al, glass, glass-ceramic, plastic/polymer material, ceramic, glass-polymer or composite materials.

[0040] The magnetic recording medium has a remanent coercivity of about 5,000 to about 10,000 Oersted, and an Mrt (product of remanance, Mr, and magnetic layer thickness, (t) of about 0.2 to about 2.0 memu/cm<sup>2</sup>. In a preferred embodiment, the Mrt is about 0.25 to about 1 memu/cm<sup>2</sup>.

### Examples

[0041] The examples relate to a method and apparatus for a magnetic recording medium with a magnetic layer having high Ms and low noise. All samples described in this disclosure could be fabricated by sputtering such as CVD, ion beam, or DC magnetron sputtering.

[0042] Examples of the film structure of the magnetic recording medium in accordance with the present invention are shown in Figures 5. In one embodiment (Figure 5a) an hcp layer having a {0002} lattice parameter and a <0002> growth

orientation is deposited upon an amorphous metallic underlayer on a substrate. An example of such a structure is a Ru alloy deposited upon an amorphous TiCr alloy. A material having a  $\{111\}$  lattice parameter similar to the  $\{0002\}$  lattice parameter, and capable of transforming into an ordered  $L_{10}$  structure is deposited with a  $\langle 111 \rangle$  growth orientation. Examples of such materials are substantially equiatomic CoPt, FePt, CoPd, and FePd alloys. Such materials may be deposited as a single layer or a multilayer of disparate composition such as single elements. The canted  $L_{10}$  structure is then formed by annealing, so that the magnetically easy  $L_{10}$   $\langle 001 \rangle$  direction is tilted parallel to a prior fcc  $\langle 001 \rangle$  cube face direction, and away from the prior vertical fcc  $\langle 111 \rangle$  growth direction.

**[0043]** In a second embodiment (Figure 5b) an fcc layer having a first  $\{111\}$  lattice parameter and a  $\langle 111 \rangle$  growth orientation is deposited upon an amorphous metallic underlayer on a substrate. An example of such a structure is one of an Ag, a Pt, and a Pd alloy deposited upon an amorphous TiCr alloy. A material having a second  $\{111\}$  lattice parameter similar to the first  $\{111\}$  lattice parameter, and capable of transforming into an ordered  $L_{10}$  structure is deposited with a  $\langle 111 \rangle$  growth orientation. Examples of such materials are substantially equiatomic CoPt, FePt, CoPd, and FePd alloys. Such materials may be deposited as a single layer or a multilayer of disparate composition such as single elements. The canted  $L_{10}$  structure is then formed by annealing, so that the magnetically easy  $\langle 001 \rangle$  direction is tilted parallel to a prior fcc  $\langle 001 \rangle$  cube face direction, and away from the vertical  $\langle 111 \rangle$  direction.

**[0044]** In these examples, the close-packed planes of the underlayer match very well with the closest-packed planes of the  $L_{10}$  structure with less than 10%, and in most cases,

less than 6% mismatch. One measure of mismatch between two materials containing such close-packed or nearly close-packed planes is  $2*(s_1-s_2)/(s_1+s_2)$ , where  $s_1$  and  $s_2$  are the nearest-neighbor atomic spacings in each material. Also, the magnetic layer according to these examples contains more than about two-thirds of its grains having a tilted c-axis and an  $L_{10}$  structure, the remaining grains having an fcc structure. In other embodiments, the magnetic layer contains more than 75% grains having  $L_{10}$  structure, the remaining grains having an fcc structure. Preferably, the magnetic layer should contain more than 85% to 95% grains having  $L_{10}$  structure, the remaining grains having an fcc structure. Preferably substantially all grains are oriented with a tilted c-axis.

**[0045]** The steps for manufacturing the medium are: (1) Depositing an underlayer for  $L_{10}$  precursor growth, having a basal plane lattice parameter similar to the  $\{111\}$  lattice parameter of the  $L_{10}$  precursor magnetic layer to be used, and orienting underlayer(s) on a substrate. (2) Depositing an alloy capable of transforming into an  $L_{10}$  structure with a  $\langle 111 \rangle$  growth orientation, to form the magnetic layer.  $L_{10}$  structure generally requires nearly equiatomic alloys or mixtures where one atom or type of atom takes “A” sites and the other atom type takes “B” sites. Example mixtures include  $Fe_{25}Co_{25}Pt_{50}$ , where Fe and Co atoms take “A” sites while Pt takes on “B” sites; and  $Fe_{50}Pt_{40}Pd_{10}$ , where Fe fills “A” sites and Pt and Pd share “B” sites. This is the ordering process. (3) Annealing as necessary to form the  $L_{10}$  ordered structure, with  $\langle 001 \rangle$  axis canted at about  $55^\circ$  away from the  $\langle 111 \rangle$  growth orientation. (4) Depositing a protective overcoat. The annealing temperature would be in the range of about 400-1,400°C, preferably about 500-600°C. Annealing time could vary from 10 seconds to 12 hours, preferably for shorter times to increase throughput and reduce grain growth.

**[0049]** The above description is presented to enable a person skilled in the art to make and use the invention, and is provided in the context of a particular application and its requirements. Various modifications to the preferred embodiments will be readily apparent to those skilled in the art, and the generic principles defined herein may be applied to other embodiments and applications without departing from the spirit and scope of the invention. Thus, this invention is not intended to be limited to the embodiments shown, but is to be accorded the widest scope consistent with the principles and features disclosed herein.

**[0050]** This application discloses several numerical range limitations that can be practiced throughout the disclosed numerical ranges. Finally, the entire disclosure of the patents and publications referred in this application are hereby incorporated herein by reference.